

Research Article

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Tattoo-like epidermal electronics as skin sensors for human-machine interfaces

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Abstract

Flexible electronic skin (e-skin) has been successfully utilized in diverse applications, including prosthesis sensing, body-motion monitoring and human-machine interfaces, due to its excellent mechanical properties and electrical characteristics. However, current e-skins are still relatively thick ($> 10 \mu\text{m}$) and uncomfortable for long-term usage on the human body. Herein, an ultrathin skin-integrated strain sensor with miniaturized dimensions, based on the piezoresistive effect, with excellent stability and robustness, is introduced. The fractal curve-shaped Au electrode in a serpentine format, which is the dominant component of the strain sensor, is sensitive to ambient strain variations and can turn the mechanical motion into a stable electrical signal output. With the advanced design of metallic electrodes, the device presents good operational stability and excellent mechanical tolerance towards bending, stretching and twisting. The stain sensor allows intimate mounting onto the human epidermal surface for the detection of body motion. By adopting a liquid bandage as an encapsulation layer, the device exhibits an ultrathin thickness ($6.2 \mu\text{m}$), high sensitivity towards mechanical deformations and capability for the clear



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detection of motion, such as walking, finger bending and the human pulse rate with identifiable electrical signals. Furthermore, the tattoo-like strain sensor is applied in robotic control by tracing finger bending motion and results in the smooth control of a robotic hand nearly without any detention. This e-skin design exhibits excellent potential for wearable electronics and human-machine interfaces.

Keywords: Skin-integrated electronics, ultrathin, excellent repeatability, fractal design, stretchable electronics

INTRODUCTION

Recently, epidermal electronics have attracted significant attention globally as a result of their excellent mechanical properties and electronic characteristics^[1-10]. Until now, extensive flexible strain sensors have been developed based on various operational principles, such as piezoelectricity^[11-14], triboelectricity^[15-17], piezoresistivity^[18-21,22]. Among the reported strain sensors, piezoelectric and triboelectric devices have raised extremely high interests for their natural characteristics in self-powering^[23-31]. However, the instantaneous electrical signals and fast attenuation of electrical performance significantly limit their further development in the application of electronic skin (e-skin)^[32]. Distinguished from self-powered strain sensors, e-skin, based on the piezoresistive effect, provides functions closer to human skin, capable of the accurate real-time detection of strain variations^[33-38]. The resistance change of the piezoresistivity in e-skin can be conveniently transformed into voltage changes via real-time electrical monitoring of the sensor, which is then recognized by a microcontroller for later robotic control.

Benefitting from the fast development of materials science, many piezoresistive effect-based e-skins have been reported by incorporating advanced conductive materials, such as graphene and polydimethylsiloxane (PDMS) composites^[39-42], ion-conducting hydrogels^[43-45] and graphene-coated fabrics^[46-48]. To achieve sufficient repeatability and stability, the fabrication process of newly-developed materials tends to require expensive equipment and rigorous experimental environments, which are not readily available with standard facilities in academic cleanrooms. Compared to these strain sensors, e-skins based on metal electrodes can realize low-cost fabrication, as well as high stability and repeatability with sufficient electrical sensitivity^[48]. As a noble metal, gold (Au) exhibits high oxidation resistance suitable for fabricating strain sensors^[49,50]. To realize its long-term utilization on the surface of human skin, e-skin must be extremely lightweight with imperceptible architectures and without any limitation and influence on body motion. It also requires skin-compatible interfaces with the targeted skin with a soft, curved dynamic surface in a stable, safe fashion that does not easily split away from the skin surface, as well as outstanding operational performance characteristics with high sensitivity and accuracy.

Herein, we report an ultrathin skin-integrated strain sensor based on the piezoresistive effect with excellent stability and repeatability. The key component is the Au electrode in the format of a fractal curve that is sensitive to ambient strain variations. To minimize the effect of the device on the skin strain field distribution, the overall dimensions of the sensor are 5 mm × 2 mm × 6.2 μm (length × width × thickness) with a mass of 0.204 mg. Compared with conventional strain sensors based on the piezoresistive effect, our strain sensor demonstrates significantly reduced dimensions with a competitive stretching range and sensitivity [Supplementary Table 1]^[51-56]. Guided by theoretical modeling, the advanced structural design enables conformal integration with the skin under large mechanical deformations. In order to yield the intimate contact on complex textures of epidermal surfaces, a liquid bandage is sprayed as a connection layer between the sensors and the epidermal surface. Compared to the commonly adopted PDMS layer, the liquid bandage possesses the advantages of low thickness (1 μm) and lightweight. The tight bondage between the sensors and the epidermal surface allows the users' unhindered movements and providing

precise measurements of the body motions sensing in a highly accurate approach. By accurately capturing finger motions and pulse rate, the sensor provides a promising alternative for real-time monitoring human health. In addition, with signals obtained from the strain sensors, a six-degree-of-freedom prosthetic arm is then used to imitate the motion of the human hand, by applying to program for sensitivity and detection adjustment.

RESULTS AND DISCUSSION

Figure 1A presents a schematic of the strain sensor. To ensure the surface smoothness and the fabrication compatibility, a quartz glass was first used as the substrate, with a spin coated poly(methyl methacrylate) (PMMA) thin film on top as a sacrificial layer and a thin polyimide (PI) film as the metal electrode supporting layer. Metallic layers (Cr/Au) were deposited on the PI film and patterned by photolithography, serving as the functional electrode for strain change detection. Spin-casting another PI film and selectively dry etching by reactive ion etching provided a top encapsulation layer for building a robust system. Dissolving the PMMA with acetone enabled transfer printing of the electrode onto the targeted skin area with pre-sprayed liquid bandage through a water-soluble tape (WST). Finally, an additional layer of liquid bandage was sprayed on top of the electronics to encapsulate the exposed gold electrode. The device features by the filamentary fractal design of the gold electrode (200 nm) and an ultrathin and stretchable encapsulation layer (liquid bandage, 1 μm) to enhance the overall flexibility and biaxial stretchability of the system [**Figure 1B**].

The liquid bandage acts as a tight adhesive and robust encapsulation for the strain sensor. A sensor is mounted on a volunteer's forearm over 12 h and during this period, the volunteer is allowed to perform all daily movements, such as walking, running and twisting his forearm. After 12 h, the sensor is still mounted on their forearm with no evidence of flaking. According to the experimental studies, the ultrathin encapsulation layers can provide an excellent protection of the gold electrode underneath and the sensor could endure various mechanical forces, like continuous rubbing, while remaining undamaged [**Supplementary Movie 1**]. Apart from the external loads, the liquid bandage is waterproof, which could protect the sensor in moisture environments. There is experimental study proves that, with the encapsulation of the liquid bandage, the sensor is approximately unaffected in a watery environment, where the change in the electrical signal ($\Delta R/R_0$) is less than $\pm 0.02\%$ [**Supplementary Figure 1**]. This tight adhesion and waterproof capability of the liquid bandage allow the strain sensor to work unaffected under large body movements and a sweated skin surface.

The overall dimensions of the strain sensor are 5 mm \times 2 mm \times 6.2 μm (length \times width \times thickness), thereby making it convenient and comfortable when attached to the human body, as shown in **Figure 1C**. Compared with recently reported piezoresistive strain sensors, our device demonstrates superior dimensions with a competitive stretching range and sensitivity, as shown in **Supplementary Table 1**. The ultrathin design combined with filamentary fractal Au wires allows the device to be stretched, bent and twisted for the seamless and conformal integration onto curvilinear surfaces of human epidermis [**Figure 1D** and **E**]. It is found that most of the skin surface would stretch within 20%, without any external stretching [**Supplementary Table 2**], indicating that the strain sensor could be mounted on most of the body parts for the body movement monitoring. Finite element analysis shows that the maximum equivalent strain in Au is less than a yield strain of 0.3% for the device under 280° of bending (bending radius of ~ 2.7 mm), 20% stretching and 90° of twisting [**Figure 1D**]. These results highlight that this robust and stretchable device can operate under realistic physiological loads.

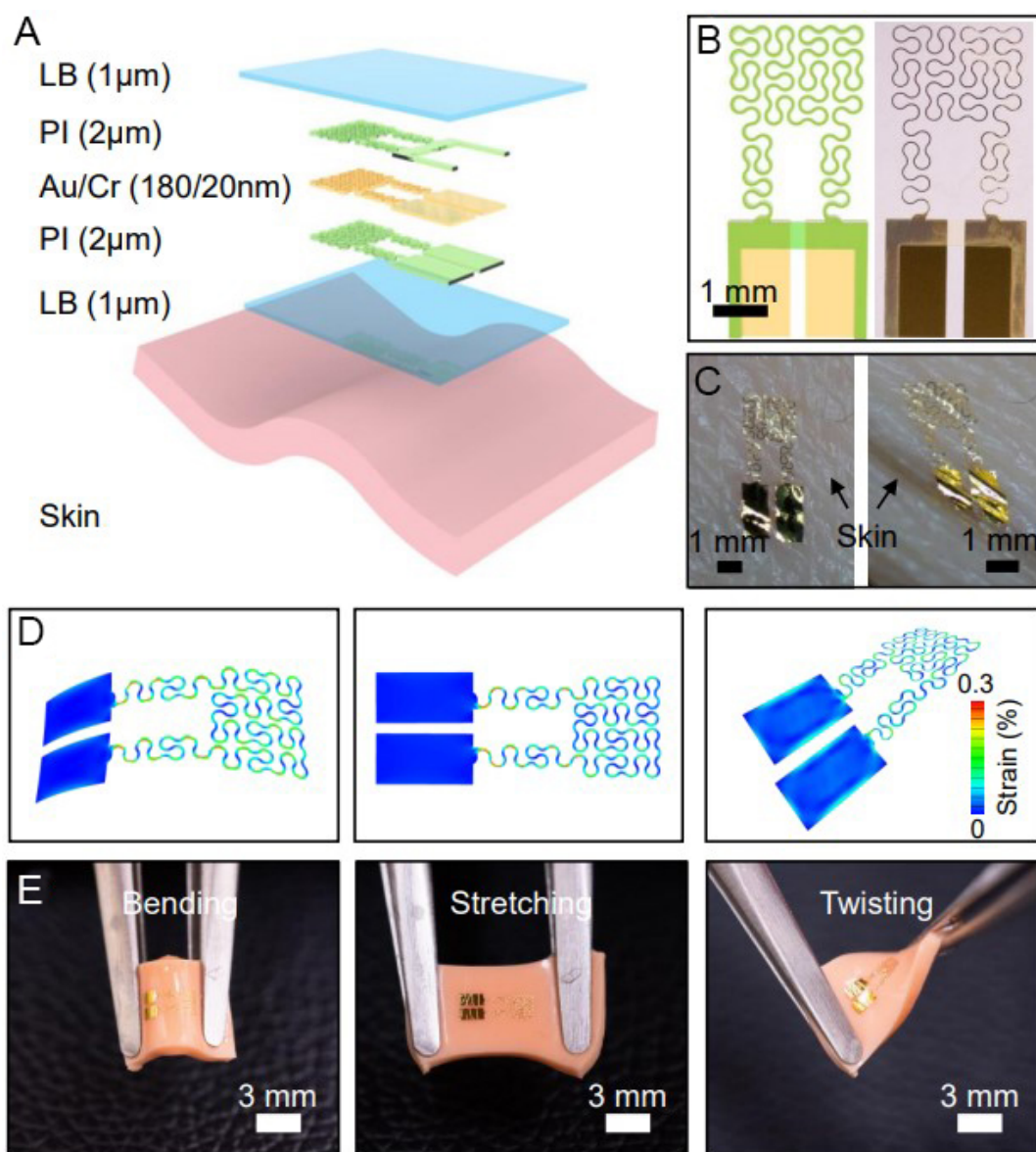


Figure 1. Flexible, ultrathin, skin-integrated and Au-based strain sensor. (A) Schematic of strain sensor. (B) Optical image of patterned Au/Cr electrode design. (C) Optical image of strain sensor mounted on the human epidermal surface. (D) Finite element analysis of strain distribution on strain sensor under stretching, twisting and bending. (E) Optical image of strain sensor attached on a pink PDMS surface with three mechanical deformations, including bending, stretching and twisting.

Figure 2A and B present the electrical signal ($\Delta R/R_0$) as a function of strain variation under the static state along length and width, respectively. It is obvious that the electrical response increases linearly with increasing strain along the two directions. At the strain change of 20%, the values of $\Delta R/R_0$ can reach 0.76% and 0.61% under longitudinal and transverse tensions, respectively. It is proved that the strain sensor is sensitive to both longitudinal and transverse strain and it is able to function at 20% strain in either direction. To investigate the frequency effect on the electrical signal, the device was tested under a constant strain variation (12.5%) with different frequencies from 1 to 6 Hz, fully covering the frequencies triggered by human daily motions, as shown in Figure 2C. It is found that the low frequency has no effect on the electrical response of the device due to its fast response time (0.04 s) [Figure 2D]. To demonstrate the high durability of the strain sensor, fatigue tests were conducted with repeated stretching for 150 cycles at 1 Hz

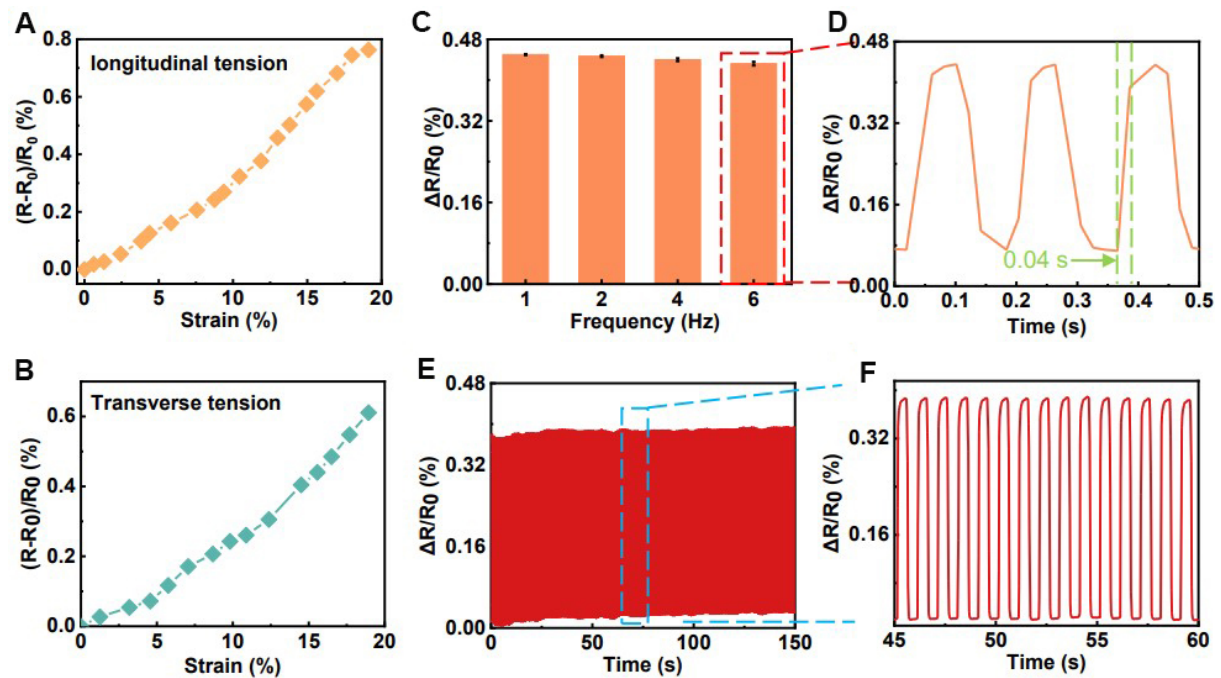


Figure 2. Electrical characteristics of strain sensor. (A) Electrical signals ($\Delta R/R_0$) of strain sensor at different longitudinal tensions. (B) Electrical signals ($\Delta R/R_0$) of strain sensor at different transverse tensions. (C, D) Electrical signals ($\Delta R/R_0$) of strain sensor at different frequencies under 12.5% strain and its detailed signals at 6 Hz. (E, F) Electrical signals ($\Delta R/R_0$) of strain sensor in a fatigue test for 150 cycles and its detailed signals from a selected range.

under 11.8% strain [Figure 2E] with electrical signals ranging from 0% to 0.4% [Figure 2F]. The results prove that the strain sensor is sufficiently durable to endure highly intensive stretching and maintain stable electrical signal outputs.

To further demonstrate its meticulous structure, the sensor is mounted on the back of a hand [Figure 3A]. Due to its ultrathin thickness and good adhesion of the encapsulation layer, the device can be conformally mounted onto human skin without any delamination during stretching. As shown in Figure 3B, the electrical signals ($\Delta R/R_0$) at bending angles of 38° , 61° and 90° are 0.121%, 0.285% and 0.567%, respectively. This proves that the strain sensor is capable of capturing small body movements and output obvious signals, which are later applied in robotics control. As shown in Figure 3C and D, a sensor is attached onto an experimenter's wrist for pulse rate recording (given with its circuit diagram), where the measured relative voltage shows a regular variation ranging from 0% to 0.073%, along with the pulse rate. It is sensitive towards the human pulse, which demonstrates the potential of the flexible skin-integrated sensors in the fields of clinical application. In Figure 3E, it shows an optical image of the strain sensor mounted on a volunteer's ankle for his walking motion detection. The $\Delta R/R_0$ varies along with the paces, ranging from 0.0173% to 0.354% [Figure 3F], which shows its capability of human motion capturing. Its sensitivity toward muscle contraction could be possibly applied in the field of motion detection in sports.

Next, the strain sensor is applied for human-machine interfaces by demonstrating the robotic hand control. The schematic of the testing circuit is shown in Figure 4A, in which the control system is composed with six strain sensors and their corresponding amplifiers (INA828, Texas Instruments) and an Arduino board. Figure 4B and C show the optical images of the strain sensors mounted on the joints of a hand and circuits connected with the Arduino board (Arduino nano with ATMEGA328P-MU chip), respectively. Those

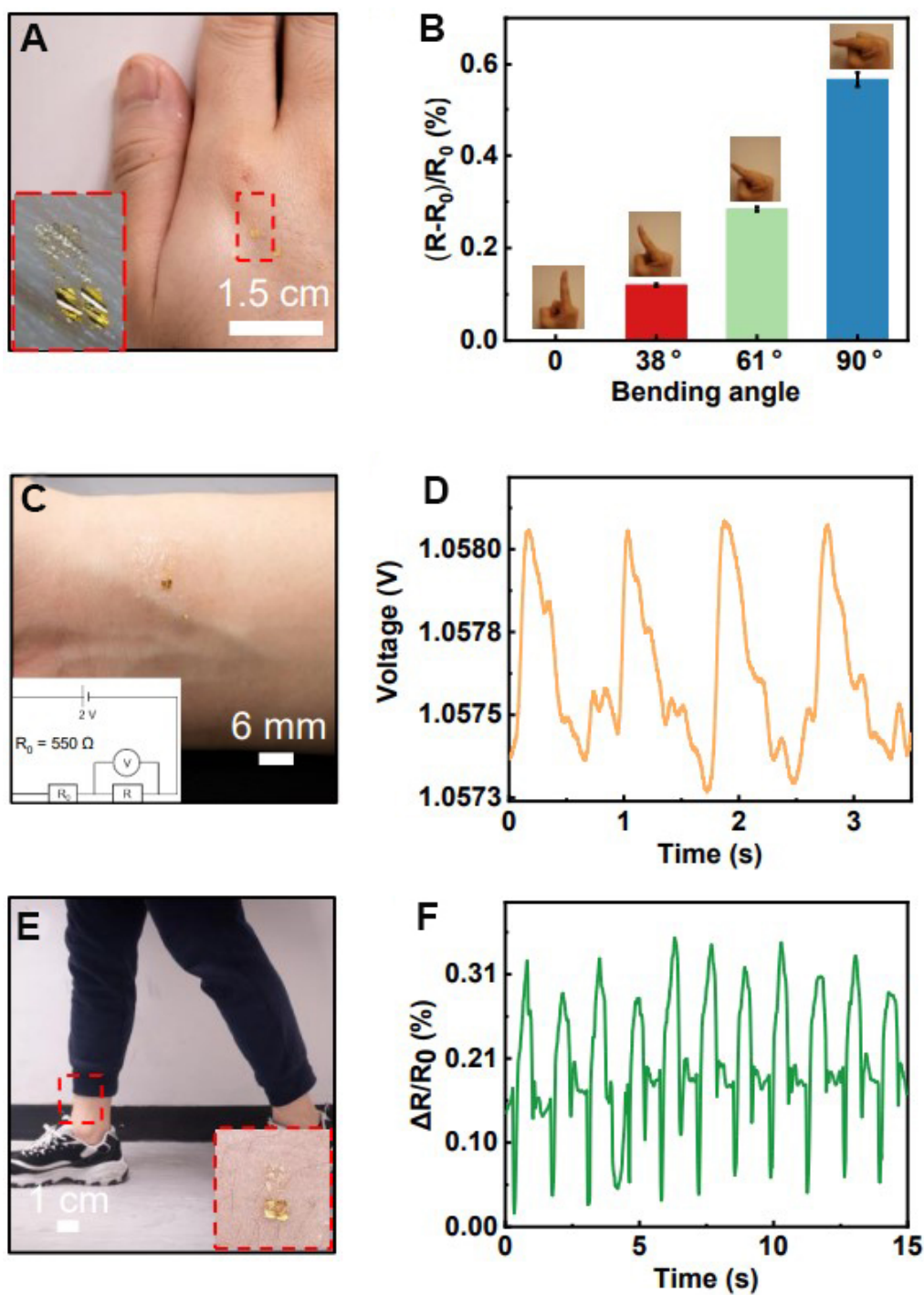


Figure 3. Electrical signals of flexible strain sensor under different external stimuli. (A) Optical image of strain sensor mounted on the back of a hand and its enlarged optical image of the strain sensor during deformation. (B) Electrical signals ($\Delta R/R_0$) of strain sensor under different finger bending angles. (C) Optical image of strain sensor mounted on a wrist for human pulse rate detection and its electrical diagram. (D) Electrical signals (V) of strain sensor in the pulse rate test in (C). (E) Optical image of strain sensor mounted on a waist for ankle for walking motion detection. (F) Electrical signals ($\Delta R/R_0$) of strain sensor under the walking motion test.

sensors are mounted on the joints of the hand to capture the finger motions, which lead to a smooth control of the robotic hand. It is able to imitate the gestures of the hand almost without any detention. In [Figure 4D](#),

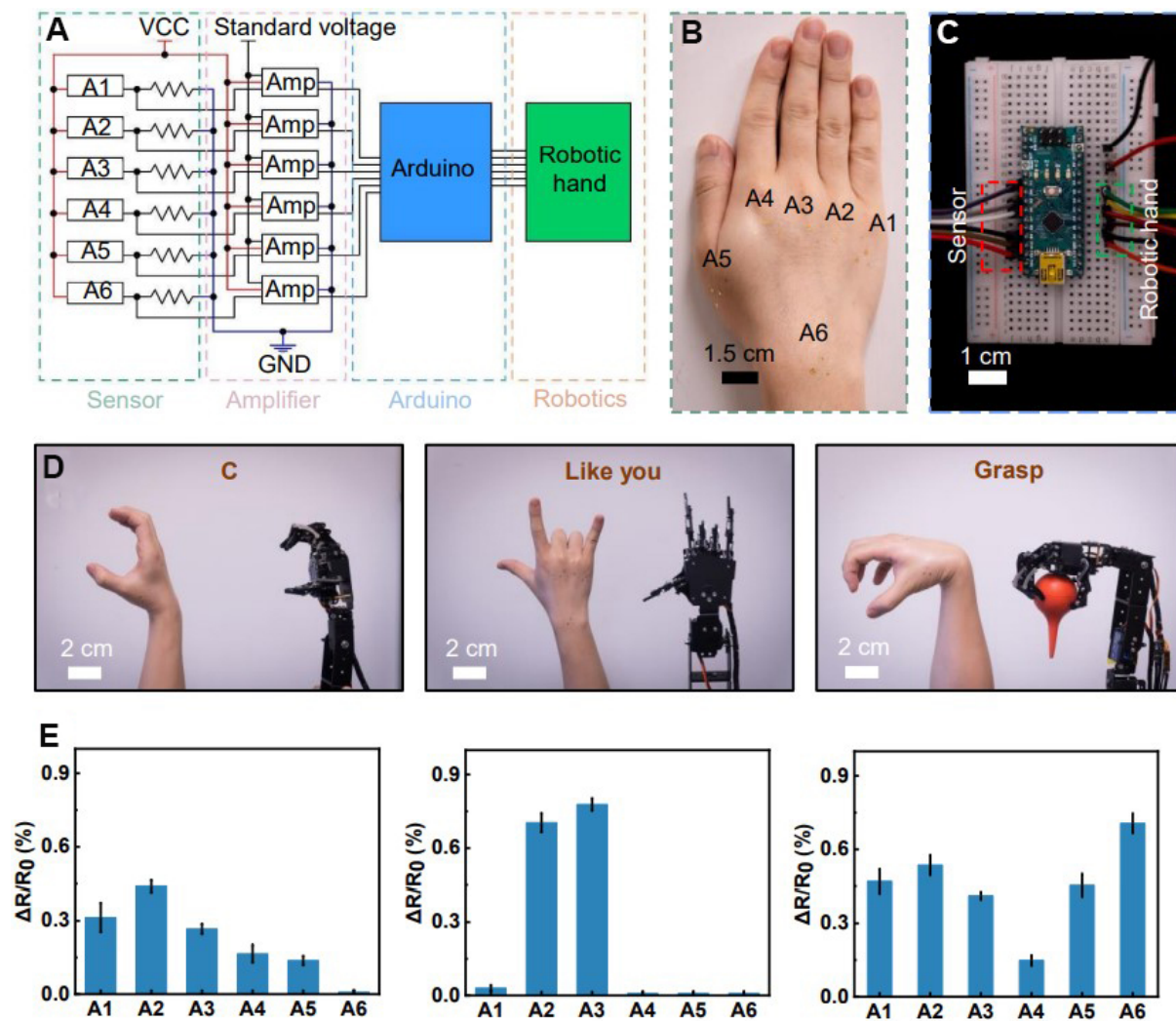


Figure 4. Robotic hand controlling performed by flexible strain sensors. (A) Schematic diagram of testing circuit for controlling robotic hand. (B) Optical image of six sensors mounted on the joints of a hand for robotic hand control. (C) Optical image of Arduino breadboard linked with the sensors and the robotic hand. (D) Optical image illustrating that the sensors control the robotic hand to make gestures of “C”, “like you” and “grasp” and their corresponding electrical signals ($\Delta R/R_0$) of sensors at different gestures (E).

some meaningful hand gestures, including “C”, “like you”, and “grasp”, are demonstrated, which proves the high feasibility of robotic hand control. Moreover, there are three corresponding graphs underneath illustrating the electrical responses of the sensors for different hand gestures. This demonstrates that the signal intensity varies with the hand’s bending degree that at the fingers’ complete bending and straightening conditions, the electrical signals ($\Delta R/R_0$) are 0.75% and 0.04%, respectively [Figure 4E]. This distinct disparity of the electrical signals leads to the accurate control of the robotic hand. To summarize, we have demonstrated a human-machine interface application of the strain sensor by controlling a robotic hand in a natural and smooth approach, thereby indicating the high feasibility of applying flexible strain sensors in human-machine interfaces.

CONCLUSION

An ultrathin Au-based stretchable strain sensor has been developed for body motion caption and human-machine interfaces. It possesses the advantages of miniaturized dimensions (5 mm × 2 mm × 6.2 μm), skin

integrability, high stability and stretchability, which allow it to be tightly mounted on the epidermal surface for body motion capturing. Its electrical signal output $\Delta R/R_0$ can rise to 0.76% and 0.61% under 20% longitudinal and transverse stretching rate, respectively, and it can undergo repeated stretching for 150 cycles at 1 Hz under 11.8% strain. With a liquid bandage as the encapsulation, the strain sensor can be tightly mounted on epidermal surface that can measure the human pulse rate and the walking motions. Furthermore, the strain sensors are applied in robotic hand control, which can imitate the finger motions of the human hand precisely, smoothly, and almost without any detention. The results in this work present the potential in body motion measuring and robotic control, which indicates a new strategy for flexible sensors in clinical applications and human-machine interfaces.

EXPERIMENTAL

Assembly of tattoo-like e-skin

First, a quartz glass was cleaned with acetone, ethanol and deionized water sequentially. Then, a PMMA solution (20 mg/mL) was spin-coated onto the surface of the cleaned glass at 2000 rpm for 30 s and then baked on a hotplate at 200 °C for 20 min. The PMMA thin film served as a sacrificial layer. Afterwards, polyamic acid solution (12.0 wt.% \pm 0.5 wt.%, 3 μ m) was spin-coated on the PMMA sacrificial layer at 3000 rpm for 30 s. The PI thin film was then cured on the hotplate at 250 °C for 30 min to densify. Cr (40 nm) and Au (200 nm) were next deposited on the PI film by magnetron sputtering, patterned with photolithography and further wet etched to form the desired pattern. The photolithography process was carried out by exposing the pre-spin-coated (3000 rpm, 30 s) and soft-baked (110 °C, 3 min) positive photoresist (PR, AZ 5214, AZ Electronic Materials) to ultraviolet light for 5 s. The pattern was then developed in an AZ 300MIF developer for 15 s, followed by a post bake at 110 °C for 3 min.

After etching the Au/Cr layer, the PR was removed with acetone and rinsed with deionized water. A second layer of PI thin film (2 μ m) was then spin coated (3000 rpm, 30 s) and annealed (250 °C, 30 min), followed by selectively dry etching (Oxford Plasma-Therm 790 RIE system, 200 W, 10 min). The patterned PI thin film served as the encapsulation layer covering the whole interconnects except the electrode areas. Next, the sample was immersed in acetone for 12 h to fully dissolve the PMMA layer. WSTs were utilized as a stamp to pick up the prepared pattern. An ultrathin layer of liquid bandage (1 μ m, Banitore company) was sprayed on the target area of human skin. Tightly attaching the WSTs on the target area then dried in the air at 25 °C for 5 min formed strong mechanical bonding. Immersing the sample in water to remove the WSTs and realize stretchable electrodes on human skin. Next, a liquid bandage layer (1 μ m) was sprayed on the top of the electrode. The liquid bandage was dried in air for 5 min to form a robust structure with strong interfacial bonding between different layers.

Characterization

The resistance was measured by a DAQ6510 data acquisition/multi-meter system. The tiny voltage variance in Figure 3D was calculated by measuring the voltage of a fixed value resistor connected in series with the triboelectric nanogenerator (the voltage was measured by PL3516/P Powerlab 16/35, which owns much lower noise signal and higher sampling rate than the DAQ6510 multimeter system).

Mechanical simulations

The finite element analysis commercial software ABAQUS (Analysis User's Manual 2016) was utilized to design the layout of strain sensor and study the corresponding mechanical performance. The objective was to decrease the strain level in Au layer under different typical loads (stretching, bending and twisting). The phantom skin was modeled by hexahedron elements (C3D8R), while the thin Au, Cr, liquid bandage and PI layers was modeled by shell elements (S4R). The minimal element size was one quarter of the width of the Au wires (50 μ m), which ensured the convergence of the mesh and the accuracy of the simulation results. The elastic modulus (E) and Poisson's ratio (ν) used in the analysis were EAu = 78 GPa, ν Au = 0.41; EPI = 2.5 GPa, ν PI = 0.34; Eskin = 60 kPa, ν skin = 0.5; EGr = 294 GPa, ν Gr = 0.21 and ELB = 85 MPa, ν LB = 0.42.

DECLARATIONS

Authors' contributions

Data curation, formal analysis, investigation, methodology, writing original draft: Wong TH

Conceptualization: Yiu CK, Zhou J

Methodology: Liu Y, Zhao L, Yoo W, Park W

Visualization: Yao K

Software and data analysis: Song Z, Xie Z

Data curation, formal analysis and supervision: Song E

Conceptualization, funding acquisition, project administration, resources, supervision and writing, review and editing: Yu X

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Conflicts of interest

All authors declared that there are no conflicts of interest.

Consent for publication

Not applicable.

Ethical approval and consent to participate

This study was conducted in accordance with the ethical guidelines and principles set forth by the Internal Review Board (IRB) of the City University of Hong Kong under approval number (HU-STA-00000850). All participants were informed about the experimental procedure and signed the informed consent forms prior to participation.

Consent for publication

Not applicable.

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