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# Energy harvesting through thermoelectrics: topological designs and materials jetting technology

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#### Abstract

The vast amount of waste heat released into the environment, from body heat to factories and boilers, can be exploited for electricity generation. Thermoelectrics is a sustainable clean energy solution that converts a heat flux directly into electrical power and *vice versa* and therefore has the potential for both energy harvesting and cooling technologies. However, the usage of thermoelectrics for large-scale applications is restrained by its device topologies and energy conversion cost efficiency trade-offs. The increase in complex topological designs reported in literature shows a shift towards customizability and improvement of thermoelectric devices for maximum energy conversion efficiency. Increasing design complexity will require an innovative, cost-effective fabrication method with design freedom capabilities. In light of this, this review paper seeks to summarize various thermoelectric topological designs as well as how 3D Printing technology can be a solution to the fabrication of cost- and performance-efficient thermoelectric devices. Specifically, as a process category of 3D Printing technology, Materials Jetting will be elaborated for its usefulness in the fabrication of thermoelectric devices. With in-depth research in materials jetting of thermoelectrics, the gap between small-scale materials research and scaled-up industry applications for energy harvesting through thermoelectric devices is expected to be bridged.



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Keywords: 3D Printing, materials jetting, thermoelectrics, topological designs, energy harvesting

#### INTRODUCTION

The escalating demand for electricity, coupled with limited reserves of fossil fuels, calls for a vital transformation toward renewable energy production. There is a pressing need for sustainable solutions to cater to our increasing electricity demands. At the same time, in factories and manufacturing processes, up to 50% of the energy consumed is released into the environment as waste heat through hot exhaust gases and liquids<sup>[1]</sup>. In the United States, 5-13 quadrillion Btu (10<sup>15</sup> Btu)/year of waste heat energy is emitted and unrecovered<sup>[1]</sup>. These copious amounts of untapped waste heat can be exploited for conversion into useful work in factories or the conversion into electrical supply. Waste-heat recovery technologies such as the Rankine cycle<sup>[2]</sup> and heat pump systems<sup>[3]</sup> often require the intermediate step of converting waste heat into mechanical energy for pumps and fans before producing useful work. On the other hand, thermoelectrics (TE) offers itself as a class of materials that inter-converts heat and electricity and thus has the ability for energy harvesting/cooling solutions. In the presence of a temperature gradient, TE materials generate an electrical potential difference, providing direct electrical energy from heat sources. The absence of moving parts allows for easy maintenance and excellent reliability while providing sustainable electrical energy to power devices. Besides harvesting waste heat from factories, heat from photovoltaic cells<sup>[4]</sup> and high-power light-emitting diodes<sup>[5]</sup> have also shown potential for energy conversion through TE devices. On a smaller scale, a small temperature difference between the human body heat (waste heat energy) and the environment is also able to generate usable energy to power wearable electronic devices<sup>[6-12]</sup>.

$$zT = \frac{S^2 \cdot \sigma \cdot T}{(k_l + k_e)}$$

where *S* is the Seebeck coefficient,  $\sigma$  is the electrical conductivity, *T* is the absolute temperature, and  $k_i$  and  $k_e$  represent the lattice and electronic thermal conductivity, respectively. A high-performance TE material should have a high power factor ( $P.F = S^2 \cdot \sigma$ ) and a low total thermal conductivity ( $k = k_i + k_e$ ). However, due to the mutual interdependency of these two properties, the optimization of *zT* is extremely difficult. Over the past decades, the enhancement of *zT* has been done primarily via engineering electronic or thermal properties. In terms of electronic properties, strategies such as band engineering and resonant doping are popular in improving the power factor<sup>[13-15]</sup>. Improvement of thermal properties can be achieved through the suppression of  $k_i$  using point defect scattering, nano-structuring, and lattice anharmonicity<sup>[16-21]</sup>. Low thermal conductivity often originates from the result of weak chemical bonding, which in turn affects the mechanical strength of the TE material. Specifically, for a thermoelectric generator (TEG), the efficiency of the heat-to-power conversion ( $\eta$ ) is expressed as:

$$\eta = \frac{T_H - T_C}{T_H} \cdot \frac{\sqrt{1 + z T_{avg}} - 1}{\sqrt{1 + z T_{avg}} + \frac{T_C}{T_H}}$$

On each end of a TEG device, it will be subjected to a hot and cold side. The  $zT_{avg}$  is the average figure of merit between the hot side temperature ( $T_H$ ) and the cold side temperature ( $T_c$ ).

Optimizing zT involves judicious materials selection and, importantly, well-designed fabrication processes<sup>[22,23]</sup>. The overall device architecture/topology is also an important aspect of efficient structural

behavior and application-focused usage. Current fabrication methods of fabricating TE legs are via spark plasma sintering and hot pressing<sup>[24-27]</sup>. These methods produce bulk TE ingots, thus restricting the geometrical complexity and the eventual energy harvesting/cooling application areas. TE device topologies need to be customizable and varied in order to increase the utilization of thermoelectric devices for different applications. As such, to increase the complexity of TE device topologies and its fabrication freedom, 3D printing is an attractive alternative fabrication method. Therefore, in this review, the applications of thermoelectrics with different topological designs will be discussed, along with their advantages and limitations. Specifically, planar TE designs will be highlighted for their usefulness for wearable self-powered electronics. To ease the processing costs and increase the material efficiency, 3D printing technology will be introduced as an emerging technique for cost-effective fabrication of thermoelectrics. Due to the rising trend of electronics 3D printing through Materials Jetting (MJ) technology, emphasis will be placed on the materials selection for materials jetted TE and the ink properties for a successful printing. Lastly, the outlook in the field of materials jetted TE for energy harvesting applications will be discussed.

#### TOPOLOGICAL DESIGNS FOR THERMOELECTRICS

There are two main topologies for TE devices, namely the vertical (or sometimes referred to as " $\pi$ ") and planar (or "lateral") arrangement of the thermopile, as illustrated in Figure 1. In both arrangements, the legs (also known as thermocouples) are made of alternating p-type and n-type thermoelectric materials and connected electrically in series and thermally in parallel.

In a vertical TEG design, thermocouples are arranged vertically along the heat flow direction  $Q_h-Q_c$  [Figure 1A]. The effective temperature gradient which gives rise to the Seebeck effect of the TEG is expressed as  $\Delta T_e$  (i.e., the difference in temperature of the hot and cold side). Vertical TEGs have high thermocouple integration and generate a high output power<sup>[28]</sup>. In comparison, vertical thermoelectric coolers (TECs) operate according to the Peltier effect, whereby a passing current creates a temperature difference across the thermoelectric device. Thus, TECs are most commonly used as Peltier modules for refrigeration in chillers, DC machines and power plants<sup>[29]</sup>. Conventional vertical TEGs and TECs are assembled via wire cutting and soldering of the metal interconnects between each thermocouple.

On the other hand, thermocouples in a planar TEG/TEC are deposited on substrates in the direction of lateral heat flow  $Q_h - Q_c$  [Figure 1B]. Compared to the vertical arrangement, a planar arrangement benefits from its fabrication adaptability and versatility on many substrates (IC chips, flexible substrates, curvatures, and textiles). Therefore, planar design finds its usefulness as micro-coolers and microgenerators in the electronics industry and wearables applications. This design is especially useful for waste body heat harvesting to self-power electronics. Conventionally, planar TE devices are fabricated via screen printing<sup>[30,31]</sup>, electrochemical deposition<sup>[32,33]</sup> and physical vapor deposition such as co-evaporation<sup>[34,35]</sup> and magnetron sputtering<sup>[36,37]</sup>.

It should also be noted that, in addition to the conventional TE designs, unique device architectures have been developed in recent years, which could lead to material-efficient devices with maximized power output. For example, O'Connor and colleagues demonstrated a new thin-film thermoelectric architecture that combines the merits of both a vertical and planar TE device, as shown in Figure  $2A^{[38]}$ . The corrugated design allows a substantial temperature difference across the thermoelectric leg. Finite element computational models of trapezoidal wave structures were developed to study the effect of geometric parameters of the corrugated TE design on thermoelectric cooling performance. The study shows that with design geometry optimization, the corrugated device has comparable performance to conventional thermoelectric materials and has high potential for flexible device applications. In another work, Lemmer



Figure 1. Topological designs and schematic diagrams of heat flow for (A) vertical design, and (B) planar design of thermoelectric devices.

and colleagues introduced the concept of origami TEGs whereby the folding of the substrates provide electrical insulation between TE elements without the need for a flexible polymer matrix as the insulating material, thus reducing the device's parasitic thermal conductance [Figure 2B]<sup>[39]</sup>. By altering the print layout, maximum power output can be achieved via thermal impedance matching of the TEG to the heat source and heat sink. In addition, Y-type TE structures were proposed by Ono and colleagues [Figure 2C]<sup>[40]</sup>. With the Y-type TE structures, heat is conducted vertically while temperature difference can be harvested in the lateral direction, allowing more thermal energy to be scavenged compared to vertical TE structures. Lastly, in Figure 2D, Snyder and colleagues fabricated stretchable TEG textiles with different configurations through the versatile weaving of TE loops<sup>[41]</sup>. The TEG textiles demonstrated stable TE performance when stretched in both the transverse and longitudinal directions. These examples illustrate the concept beyond conventional vertical and planar TE structures - which is feasible and an improvement over the well-established field of TE structures. However, the fabrication process is tedious and limits its wide adoption industrially.

## ADDITIVE MANUFACTURING FOR FABRICATION OF COMPLEX THERMOELECTRIC STRUCTURES

To increase the industrial implementation of energy harvesting through TE devices, its processing costs and energy conversion performance must be competitive. Compared to labor-intensive conventional fabrication routes, Additive Manufacturing (AM) is a fitting manufacturing technology for the advancement of costeffective high-performance TE devices. Coupled with minimal material wastage, high-throughput process and geometrical flexibility, it is timely and appropriate for extensive research into additively manufactured thermoelectrics. To expedite this research area, it is important to understand the different AM technologies, with their merits and weakness, as a methodological approach in effectuating additive manufactured thermoelectrics for industrial applications.



**Figure 2.** Nonconventional thermoelectric device topologies reported in recent years. (A) Corrugated TEG, adapted with permission from<sup>[38]</sup>, (B) Origami TEG, adapted with permission from<sup>[39]</sup>, (C) Y-type TEG, adapted with permission from<sup>[40]</sup> and (D) woven interlocking TEG, adapted with permission from<sup>[41]</sup>.

As shown in Figure 3, AM technology can be broadly classified into 7 main process categories - Binder Jetting, Directed Energy Deposition (DED), Material Extrusion, Material Jetting (MJ), Powder Bed Fusion (PBF), Sheet Lamination and Vat Photopolymerization (VP). Each process has found its influence in several major applications. For instance, in dentistry, VP has seen exponential interest and utilization. The significant reduction in manufacturing time for bridges and crowns, coupled with its excellent surface finishing and resolution, has led to the adoption of VP in many dental clinics and laboratories<sup>[42,43]</sup>. DED and PBF techniques have already been used extensively to manufacture customized metal parts in the repair of aerospace components<sup>[44]</sup>. However, as compared to Materials Extrusion and MJ technology, DED and PBF have higher equipment costs due to their system requirements. In relation to thermoelectrics, there is no singular AM method that can optimally print both vertical and planar TE designs. Depending on the topology of TEG for its required application, different 3D printing techniques are listed in Table 1.

Several 3D printing methods have the ability to fabricate highly hierarchical and material efficient thermocouples for vertical TE devices, as shown in Table 1. However, most of these 3D printing methods (such as PBF, DED, VP and Binder Jetting) still require post 3D printing assembly of the integrated TE device. Currently, Materials Extrusion technique is the most reported 3D printing method to print TE materials such as bismuth telluride ( $Bi_2Te_3$ )-based materials<sup>[45,46]</sup> and compositionally segmented TE legs<sup>[47]</sup>. Materials Extrusion technique also has the potential to fabricate an entire vertical TE device through

Topology	3D printing method	State of TE material feedstock	Surface finishing of printed structures	Post-printing TEG assembly required	Advantages	Disadvantages	
Vertical arrangement	Materials extrusion	Liquid- based/Filament- based	Poor	No	1. Ability to generate high electrical power	<ol> <li>Limited device flexibility</li> <li>Difficulty in reducing</li> </ol>	
	Powder bed fusion	Powder-based	Good	Yes		size due to assembly problems	
	Directed energy deposition	Powder-based	Good	Yes		3. High manufacturing costs of powder-based 3D printing methods	
	Vat photopoly- merisation	Photocurable liquid- based	Good	Yes			
	Binder jetting	Powder-based	Poor	Yes			
Planar arrangement	Material jetting	Liquid-based	Excellent	No	1. Deposition on many substrate materials	1. Difficulty in generating high temperature	
	Sheet lamination	Liquid-based	Excellent	No	(including flexible substrates) 2. Cheaper manufacturing process	difference 2. Low electrical power generated	

#### Table 1. Comparison of the 7 Additive Manufacturing process categories for the two main topologies of TE devices



Figure 3. The 7 main Additive Manufacturing process categories. Each process category has its strengths for different industrial applications.

alternating nozzle printing. However, the thermal expansion mismatch between the different materials during the heat treatment process still poses a technical challenge in multi-material 3D printing research area. Furthermore, the "stair-step" effects of Materials Extrusion technique and surface roughness of binderjetted printed parts greatly damage the resultant structural quality of 3D thermoelectrics structures.

On the other hand, techniques such as MJ and Sheet Lamination are unable to build thermocouples with a high aspect ratio. However, these techniques allow printed TEs to have high levels of printing resolution and excellent surface finishing. These techniques also show potential for the printing of integrated planar devices as they are relatively mature technologies for multi-materials fabrication. The lack of need for post-printing assembly solves a major problem in thermocouples and electrode adhesion and contact resistance required in TE assemblies. These traits thus make planar TE devices for self-powered/cooling electronics and wearable applications viable through these 3D printing fabrication methods.

More specifically, MJ has been gaining momentum as an alternative candidate in the field of electronics 3D printing due to its precise deposition and high resolution of printed features. According to ISO/ASTM 52900, MJ is defined as an additive manufacturing process in which droplets of feedstock material are selectively deposited. Within MJ, there are a few distinct techniques such as Drop-on-Demand (DoD) Inkjet Printing, Nanoparticle Jetting (NPJ), Polyjet<sup>[48]</sup> and Aerosol Jetting<sup>[49]</sup>. While Polyjet is mainly used for polymeric prototyping and tooling, DoD inkjet printing, NPJ and Aerosol Jetting have main applications in electronics material jetting. A tremendous amount of research effort has been poured into the development of flexible and stretchable nanoelectronics and bioelectronics through Materials Jetting, in particular, DoD Inkjet Printing and NPJ. DoD Inkjet Printing is an established printing technique that deposits ink via a thermal or piezoelectric system<sup>[50,51]</sup>. NPJ, on the other hand, jets inks containing metal or ceramic nanoparticles on a heated build platform, allowing the solidification of nanoparticles for better handling and post-printing treatments. Solidification of material jetted structures can range from ultra-violet light assisted, infrared light and thermal assisted<sup>[52]</sup>. In addition, there is ongoing research into reactive jetting technique to increase the printed part strength<sup>[53]</sup>. In contrast, Aerosol Jetting is a relatively newer MJ technique that has been gaining recognition as a fabrication technique for electronics printing. This dropletbased method deposits an aerodynamically focused aerosol jet stream carried from an aerosol mist reservoir<sup>[54]</sup>. This technique allows feature size of less than 10 µm with thickness from 100 nm to several millimeters, making it suitable for printing interconnects, antennas, and sensors<sup>[49]</sup>. In addition, the versatility of 5-axis systems (e.g., Optomec Aerosol Jet) has great potential for electronics printing on complex substrates and surfaces. Despite the differences in the droplet formation and solidification methods, these techniques serve to build structures from material droplets, forming the broad MJ technique process category.

#### Materials selection for materials-jetted thermoelectrics

The selection of material plays an important part in the fabrication of high-performance and flexible thermoelectric devices. For inorganic materials, 1D nanostructured materials such as nanowires, nanorods and nanotubes are preferred over powder-based materials due to several reasons. Firstly, due to the small nozzle orifice of typical inkjet printers for high-resolution printing, nanoscale TE materials are required to avoid nozzle clogging. Conventional solid-state synthesis of TE materials will result in powder-based TE material. The powder would need to undergo an additional high energy ball milling process to obtain nanosized powder, in which homogeneity of powder size may be a challenge as well. Secondly, 1D nanostructured TE materials provide opportunities to tailor both electrical and thermal conductivity properties by tuning their alignment/orientation, which can potentially increase the efficiencies of TE materials well beyond the current zT values.

There have been many studies to synthesize high performing 1D inorganic TE materials. A few examples will be elaborated on below, together with efforts to achieve flexible TE films. In Figure 4A, Dun and colleagues overcame the predicament between the low flexibility and high electrical conductivity of Tellurium (Te) nanorods via the fabrication of polyvinylidene fluoride (PVDF)-Te composite fabric<sup>[55]</sup>. The synthesized Te nanorods were < 10  $\mu$ m in length with diameter between 600-800 nm. After mixing with PVDF, the composite fabric achieved a high room temperature power factor of 45.8  $\mu$ W/mK<sup>2</sup>. This is comparable to optimized Te nanowire-PEDOT:PSS based thermoelectrics and is an order of magnitude higher than other TE nanowire-based thermoelectrics<sup>[55]</sup>. In addition, the thermoelectric fabric is scalable with good flexibility, making it a great potential for wearable electronic applications. A separate study was conducted by Park and colleagues on the fabrication of PANI-coated Ag<sub>2</sub>Se nanowires (NWs) on PVDF-based TE composite films [Figure 4B]<sup>[56]</sup>. The composite films were produced using a solution-mixing (synthesizing of Ag<sub>2</sub>Se NWs) and drop casting method (fabrication of device). The resulting Ag<sub>2</sub>Se/PVDF



**Figure 4.** Synthesis of 1-Dimensional inorganic TE materials. (A) PVDF-Te nanorods composite films, adapted with permission from<sup>[55]</sup>, (B) PANI-Ag<sub>2</sub>Se NW/PVDF films, adapted with permission from<sup>[56]</sup>, (C) Ag<sub>2</sub>Te films, adapted with permission from<sup>[57]</sup>, and (D)  $Cu_{1.75}$ Te-PVDF fabric, adapted with permission from<sup>[58]</sup>.

film exhibited a high room temperature power factor of approximately 196.6 µW/mK<sup>2</sup>. At a temperature difference of 30 K, an output voltage of 15.4 mV was generated. In addition, silver telluride (Ag<sub>2</sub>Te) NWs were also investigated due to their high power factor and low thermal conductivity. The synthesized Ag, Te NW synthesized as shown in Figure 4C exhibited a low thermal conductivity (0.08 W/mK) in the through-plane direction but has a high thermal conductivity (1.04 W/mK) in the in-plane direction<sup>[57]</sup>. After synthesizing the NWs, Ag, Te NW film was fabricated using vacuum filtration and mechanical pressing of 30 MPa pressure. This leads to good flexibility on the fabricated film, where the film can even be folded into a paper plane. In Figure 4D, Zhou *et al.* synthesized  $Cu_{1,75}$ Te NWs<sup>[58]</sup> with an average diameter of  $10 \pm 2$  nm and length of approximately 5 µm. Similarly, the NWs were vacuum-filtrated and pressed with a pressure of 30 MPa. The assembled  $Cu_{1,75}$ Te-PVDF fabric exhibited a low Seebeck coefficient but has an ultra-high electrical conductivity, with a room temperature power factor of 23  $\mu$ W/mK<sup>2</sup>. The fabric was also subjected to a bending test of 300 cycles and the thermoelectric properties did not degrade much hence, showing great potential for flexible thermoelectric applications. Despite the promising performance of 1D nanostructured TE materials, these materials are often casted, or vacuum-filtrated and pressed as films. These methods severely limit the translation to functional TE devices. As such, there is a need to advance and incorporate additive manufacturing for functional and effective 1D nanostructured TE materials and devices.

Similar to inorganic TE materials, organic TE materials (e.g., carbon nanotubes (CNT) and poly(3,4-ethylenedioxythiophene) poly(styrenesulfonate) (PEDOT:PSS)) were also extensively researched, as shown in Table 2. Compared to organic TE materials, the scarcity of elements such as Te, Gallium (Ga) and Germanium (Ge) impedes the deployment of inorganic thermoelectrics for large-scale industrial applications. As such, organic thermoelectrics offer the advantages such as elemental abundance, ease of

Table 2. Synthesis methods for organic TE materials/films that are suitable for adaptation towards Materials Jetting of TE devices				
	Power			

Method of fabrication	TE material	Additives	Thermal conductivity (W/mK)	Seebeck coefficient (µV/K)	Electrical conductivity (S/cm)	factor (μW/ mK <sup>2</sup> )	<i>zT</i> at room temp.	Ref.
Bar Coating	PEDOT:PSS, Graphene, CNT	-	0.36	23.2	689	37.08	0.031	[59]
Casting	CNT	PVA emulsion	0.34	38	48	6.9	0.006	[60]
Casting	SWCNT, PEDOT:PSS	-	0.2-0.4	18.3	400	13.4	0.02	[61]
Casting	SWCNT, Polyaniline (PANI)	-	0.43	65	769	176	0.12	[62]
Drop Casting	CNT	Benzyl viologen	5	-116	1534	3103	0.20	[63]
Drop Casting (50 % CNT composite film)	SWCNT	Poly[N-butyl-2-[5,5'-(2,5- bis(octyloxy)-1,4- phenylene)bis(thiophene-2- yl)vinyl]pyridinium iodide]	-	54	159	46.4	-	[64]
Drop Casting	DWCNT, Polyaniline	Camphorsulfonic acid	-	61	610	220	-	[65]
Drop Casting	SWCNT, PEDOT:PSS	DMSO	0.4-0.6	55.6	1701	526	0.39	[66]
Drop Casting (6.7 wt % CNT)	PEDOT:PSS, SWCNT	Formic acid	-	54	1300	407	-	[67]
Drop Casting (6.7 wt% CNT)	PEDOT:PSS, SWCNT	DMSO	-	59	1230	464	-	[67]
Floating- Catalyst Chemical Vapor Deposition	CNT, PEDOT:PSS	-	-	82.9	734.5	504.8	-	[68]
Spray Coating	SWCNT	PEI	-	-58	10	3.4	-	[69]
Spray Coating	SWCNT, Poly(3,4- ethylenedioxythiophene) (PEDOT)	Tetrakis(dimethylamino)ethylene	0.67	-1250	6.6	1050	0.5	[70]
Vacuum Filtration	DWCNT	Chlorosulfonic acid	-	18	17,400	550.8	-	[71]
Vacuum Filtration	SWCNT	Napthalene diimide	-	-55	446	135	-	[72]
Vacuum Filtration	SWCNT	Perylene diimide	-	-47.3	500	112	-	[72]
Vacuum Filtration	SWCNT	Poly-Schiff base	-	42.7-44.1	393-430	71.9- 83.5	-	[73]
Vacuum Filtration	SWCNT, Poly(3,4- ethylenedioxythiophene) (PEDOT:PF6)	-	-	51.0-56.8	1357-1531	243.3- 264.1	-	[74]
Vacuum Filtration (70 wt% SWCNT)	SWCNT, PEDOT:PSS coated Te nanorod	H <sub>2</sub> SO <sub>4</sub>	-	56	332	104	-	[75]
Wet Spinning	SWCNT, PEDOT:PSS	-	0.71	35	980	83.5	0.035	[76]
Wet Spinning	SWCNT, PEDOT:PSS	PEI	0.39	-48.2	540	126	0.096	[76]

PVA: Poly(vinyl acetate); CNT: carbon nanotubes; SWCNT: single-walled CNT; DWCNT: double-walled CNT; PEDOT:PSS: poly(3,4-ethylenedioxythiophene) poly(styrenesulfonate); DMSO: dimethyl sulfoxide; PEI: polyethylenimine; H<sub>2</sub>SO<sub>4</sub>: sulfuric acid.

processability and low toxicity for low-temperature applications. To date, organic TE materials are still fabricated into films via traditional methods such as coating<sup>[59]</sup>, casting<sup>[60-67]</sup>, chemical vapor deposition<sup>[68]</sup>, spray coating<sup>[69,70]</sup>, vacuum filtration<sup>[71-75]</sup>, and wet spinning<sup>[76]</sup>, as shown in Table 2. The integration of TE materials into devices is challenging using these methods. Based on Table 2, a peak zT of 0.5 at room temperature is achieved for CNT-PEDOT hybrid material treated with tetrakis(dimethylamino)ethylene  $(TDAE)^{[70]}$ . In comparison, inorganic TE materials such as Bi<sub>2</sub>Te<sub>3</sub>-based materials have a peak zT of > 1.0 at room temperature<sup>[77]</sup>. Besides examining zT performance at room temperature as listed in Table 2, the high melting point of organic TE materials such as CNT allows for its utilization in TE applications at higher temperatures. To further form free-standing CNT films from traditional spray coating methods, argon plasma treatment and sonication can be utilized. For instance, Zhao and colleagues investigated the effects of post treatment on the performance of free-standing CNT films and found that argon plasma treatment can significantly enhance zT performance from 0.01 to 0.4 at 675 K<sup>[78]</sup>. Overall, organic TE materials possess inherently lower thermal and electrical conductivities compared to inorganic TE materials. Nevertheless, the zT performance of organic TE materials is still significantly lower than that of inorganic TE materials. Therefore, strategies such as molecular structure modification, nanocomposites of organic/inorganic hybridization and chemical functionalization can be employed to improve zT performance of organic TE materials<sup>[79,80]</sup>.

#### Materials-jetted thermoelectrics

Individual merits of organic, inorganic, and composite TE materials have garnered considerable attention in the TE community. While these materials have been explored in bulk and thin film forms, interest has been growing, particularly for TE devices fabricated via 3D printing. 3D printing offers the capabilities of multimaterial printing for TE device fabrication. Research efforts have been channeled towards optimizing the printability of flexible, conformable devices while sustaining modest TE performance. However, not much research has been done in this field of Materials Jetted TE to date. The reported literature on materials jetted TE materials are tabulated in Table 3.

Solution-based organic TE materials alleviate the chances for clogged prints and thus increase the success rate of printed TE devices. As evidenced by the ease of solution-based organic materials printing, there are more reports on organic and composite TE materials jetting<sup>[81-85]</sup> as compared to inorganic materials jetting<sup>[86,87]</sup> as shown in Table 3. For example, Juntunen and colleagues synthesized graphene films exhibiting a room temperature Seebeck of 41  $\mu$ V/K and a power factor of 18.7  $\mu$ W/mK<sup>2</sup>, which is comparable to existing graphene-conductive polymer nanocomposites [Figure 5A]<sup>[85]</sup>. A room temperature charge carrier concentration of  $3.17 \times 10^{19}$  cm<sup>-3</sup> and a hole mobility of 21.5 cm<sup>2</sup>/Vs were also achieved. The carrier concentration value agrees with their proposed model that the films exhibited electrical transport behavior from the few-layer graphene flakes and were not influenced by the disordered structure of the film. The fabrication process via the incorporation of minute amounts of polyvinylpyrrolidone (PVP) into exfoliated graphite in IPA resulted in a well-connected 3D network printable over a large area. The resultant film also proved to be stable after 10,000 bending repetitions over a 4.5 mm radius. Similarly, in Figure 5B, Ferhat and colleagues<sup>[83]</sup> utilized inkjet printing for vanadium pentoxide (V<sub>2</sub>O<sub>5</sub>) xerogels incorporated with poly(3,4-ethylenedioxythiophene) (PEDOT). The difference in charge carriers between the organic and inorganic components upon the addition of 0.03 molar ratio of PEDOT resulted in an overall increased power factor of 2  $\mu$ W/mK<sup>2</sup>, which is much higher than the pristine V<sub>2</sub>O<sub>5</sub> film with a power factor of  $2 \times 10^{-3} \mu W/mK^2$ . The n-type (PEDOT)<sub>x</sub>V<sub>2</sub>O<sub>5</sub> thermoelectric was then paired with p-type PEDOT:PSS and printed into a flexible organic TEG.

Method of fabrication	TE material	Additives	Thermal conductivity (W/mK)	Seebeck coefficient (µV/K)	Electrical conductivity (S/cm)	Power factor (μW/mK <sup>2</sup> )	zT	Ref.
			Organic and Composites					
Aerosol Jetting	Bi <sub>2</sub> Te <sub>3</sub> - PEDOT:PSS	EG, water	-	22.5	360	~18	-	[81]
Aerosol Jetting	Sb <sub>2</sub> Te <sub>3</sub> - PEDOT:PSS	EG, water	-	33.8	247.3	28.3	-	[81]
Aerosol Jetting	Sb <sub>2</sub> Te <sub>3</sub> -MWCNTs-PEDOT:PSS	PVP, water	-	29	496	41	-	[82]
Inkjet Printing	(PEDOT) <sub>x</sub> V <sub>2</sub> O <sub>5</sub>	Triton X-100	0.68	-350	0.16	2	0.001	[83]
Inkjet Printing	Poly[Cu <sub>x</sub> (Cu-ett)]	PVDF, DMSO	-	41	5.14	0.86	-	[84]
Inkjet Printing	Poly[K <sub>x</sub> (Ni-ett)]	PVDF, DMSO	-	-44.9	2.12	0.43	-	[84]
Inkjet Printing	Graphene	PVP, IPA	-	41	-	18.7	-	[85]
			Inorganic					
Inkjet Printing	Bi <sub>2</sub> Te <sub>3</sub> NW	Water	0.193	-94.2	172.6	163	0.26	[86]
Inkjet Printing	Bi <sub>0.5</sub> Sb <sub>1.5</sub> Te <sub>3</sub> NW	Water	0.55 (in-plane)	85.7	240.8	180	0.13	[87]
Inkjet Printing	Bi <sub>2</sub> Te <sub>3</sub> NW	Water	1.19 (in-plane)	-117.2	82.0	110	0.04	[87]

#### Table 3. 3D printed TE materials fabricated via Materials Jetting

EG: Ethylene glycol; PVDF: polyvinylidene fluoride; PVP: poly(vinylpolypyrrolidone); IPA: isopropyl alcohol.

In addition to inkjet printing, aerosol jet printing is also being explored in fabricating printed composite-based thermoelectric devices. In Figure 5C, Ou and colleagues<sup>[81]</sup> reported a PEDOT:PSS matrix mixed with  $Bi_2Te_3/Sb_2Te_3$  nanoparticles to enhance the electrical transport. The incorporation of 85 wt%  $Sb_2Te_3$  nanoflakes resulted in a Seebeck coefficient of 33.8  $\mu$ V/K, and an electrical conductivity of 247.3 S/cm, ultimately demonstrating a peak power factor of 28.3  $\mu$ W/mK<sup>2</sup>. In their later study, Ou's group explored the addition of multi-walled carbon nanotubes (MWCNT) and  $Sb_2Te_3$  in PEDOT:PSS and similarly found that 85 wt% loading of  $Sb_2Te_3$  and MWCNT yielded a further improvement with a power factor of ~41  $\mu$ W/mK<sup>2[82]</sup> [Figure 5D].

From Table 3, inorganic TE NWs are promising materials to be jetted, yet there have not been many studies in this area. A study done by Chen and colleagues demonstrated the successful ink jetting of synthesized singly crystalline  $Bi_2Te_3 NWs^{[se]}$ . The  $Bi_2Te_3 NWs$  achieved a power factor of 163  $\mu$ W/mK<sup>2</sup> and *zT* of 0.26 at room temperature. For the second study, the same group achieved a high power factor of 180  $\mu$ W/mK<sup>2</sup> at 400 K for  $Bi_{0.5}Sb_{1.5}Te_3 NWs$  and 110  $\mu$ W/mK<sup>2</sup> at the same temperature was obtained for the  $Bi_2Te_3 NWs^{[se]}$ . Synthesized NWs were ink jetted onto a flexible polyimide substrate and a flexible thin-film TEG device, made up of 5 pairs of  $Bi_2Te_3$  and  $Bi_{0.5}Sb_{1.5}Te_3 NWs$ , was fabricated. An output voltage of 45 mV was achieved at a temperature difference of 32.5 K for the device. The *zT* performance of the reported jetted inorganic TE materials is at least two orders of magnitude higher than the materials jetted organic TE materials, as shown in Table 3. Despite these efforts, current materials jetted TE materials performance still pales in comparison to conventional spark plasma sintered or hot pressed TE materials<sup>[88-90]</sup>. Nonetheless, these studies suggest that MJ has high potential as a viable fabrication approach for flexible thermoelectric applications and should be further explored.



**Figure 5.** (A and B) Ink jetting of organic/composite TE devices. Figures are adapted with permission from<sup>[85]</sup>. (C and D) Aerosol jetting of composite TE devices on flexible substrates. Figures are adapted with permission from<sup>[81]</sup>.

#### Ink properties for materials-jetted thermoelectrics

To improve the current state of Materials Jetted TE technology, the necessary ink properties and printing parameters for a successful print must be well understood. Here, two ink properties - flow behavior and material curing will be discussed. Optimization of printing parameters such as the speed of jetting, input pressure, nozzle dwell time (pulse width) and number of repetitions are discussed in other papers<sup>[91,92]</sup>. The substrate property (i.e., porosity and surface tension) is also an important factor to be considered and has also been detailed in other papers<sup>[93,94]</sup>.

First, the TE ink needs to have an optimal flow behavior. For Newtonian fluids, droplet formation is determined by the dimensionless inverse (*Z*) of the Ohnesorge number (*Oh*) which is related to the Reynolds (Re) and Weber (We) numbers. The inverse of the Ohnesorge number is given by  $Z = Oh^{-1} = (a\rho\gamma)^{1/2}/\eta = \text{Re/We}^{1/2}$ , where *a* is the nozzle diameter,  $\rho$  is the density,  $\gamma$  is the surface tension and  $\eta$  is the viscosity of the fluid<sup>[95]</sup>. However, Newtonian fluids may face the problem of dispensing satellite droplets when *Z* is too high (> 10). Satellite droplets can be formed due to the fragmentation of the spherical liquid droplet upon exiting the nozzle (typically 20-50 µm in diameter<sup>[95]</sup>) and thus creating numerous splashes on the substrate, decreasing the printing resolution. To reduce satellite droplets, surfactants and long-chain macromolecules in low concentrations can be added to decrease *Z* through the increase of viscosity. The addition of these polymers gives the ink some viscoelasticity, allowing it to turn from a Newtonian fluid into a low-viscosity elastic liquid<sup>[96,97]</sup>. Surfactants also prevent particle aggregation and nozzle clogging by improving the ink colloidal stability. The influence of different fluids *Z* values on droplet formation is shown in Figure 6A-C. As studied by Jang and colleagues<sup>[95]</sup>, a fluid droplet with Z = 2.17 allows the tail of the filament to be continuously necked, forming a long fluid filament. An eventual droplet was formed around ~200 µs of elapsed time. A fluid droplet with Z = 6.57 generated both a primary droplet and



**Figure 6.** (A-C) Influence of fluid Z values on primary and satellite droplet formation. Figures are adapted with permission from<sup>[95]</sup>. (D and E) Alignment of SWCNT from "coffee rings" effects by Aerosol Jetting. Figures are adapted with permission from<sup>[101]</sup>.

a satellite droplet, which merged into a single droplet at an elapsed time of ~160  $\mu$ s. A fluid droplet with Z = 17.32 generated a primary droplet and satellite droplet. However, even after 200  $\mu$ s, the satellite droplet was unable to merge with the primary droplet. Therefore, the printability of the ink can be optimized through the tailoring of the fluid Z value.

Second, most MJ inks are water/solvent-based systems, and the primary mode of curing is through solvent evaporation. The solvent drying conditions are essential in controlling the printed morphology and microstructural porosity, and particle arrangement. The formation of "coffee rings" happens when ink is left to dry on the substrate. The phenomenon happens when solvent evaporation drives an outward radial flow, transporting material towards the periphery, causing defects and poor structural resolution<sup>[98]</sup>. To minimize the formation of "coffee rings" of ink jetted graphene oxide, Derby and He developed a model to understand the influence of substrate bed temperature, graphene oxide particle size and droplet size on the solvent evaporation<sup>[98]</sup>. Apart from controlling these parameters, adding cosolvents [such as sodium dodecyl sulfate (SDS)] changes the surface tension to promote an opposing Marangoni flow and can also alleviate "coffee ring" defects<sup>[99]</sup>. However, "offee rings" may still have their merits, particularly in the field of printed electronics. Due to the strong wettability contrast between the surface-modified hydrophobic and hydrophilic substrate regions, Takenobu and colleagues achieved highly aligned ink jetted single-walled carbon nanotubes for high-performance electronic devices<sup>[100]</sup>. In a similar vein, as shown in Figure 6D and E, Goh and colleagues have leveraged the "coffee ring" effect of aerosol jetting to preferentially align twin-lined CNT for high-speed electronic device applications<sup>[101]</sup>. Compared to water/solvent-based inks, photocurable inks has the advantage of less surface spreading due to the relatively higher viscosity. However, the curing depth is hindered by the filler's refractive index and may be a challenge for inorganic TE materials. The additional post-printing photocuring step also makes it a less time-efficient method compared to water/solvent-based ink systems.

#### CONCLUSION AND OUTLOOK

Thermoelectrics is an attractive class of material for energy harvesting and cooling technology. Particularly, thermoelectrics has garnered renewed interest as an energy harvesting material for waste heat recovery from body heat to exhaust systems. Its direct conversion from waste heat into useful electrical energy allows it to be implemented in many waste heat systems. However, due to the high processing and material cost, thermoelectrics is still limited to niche applications for remote powering in military and spacecraft systems<sup>[102]</sup>. Additive manufacturing technology, however, offers cost-effective manufacturing of thermoelectrics for industrial and wearable energy harvesting applications. The growing trend beyond conventional vertical and planar thermoelectric designs towards complex configurations for efficient heat conversion can be easily realized with additive manufacturing. Specifically, materials jetting is a fitting pillar of additive manufacturing that is well-suited for 3D printing of electronics. This facile and relatively cheap printing technique offers the advantages of multi-material printing for device fabrication with minimal inter-material delamination, thus allowing for the large-scale fabrication and automation of TE device manufacturing. The ability for substrate-based printing of two-dimensional thermoelectrics allows the flexible device to conform to host pipes and human wrists for waste heat conversion. However, with any substrate-based system, the working temperature of the printed device is limited by the substrate working temperature. Often, these are textile substrates with low degradation temperatures. Therefore, alternative substrates such as metal and ceramic for high temperature applications should be explored. Consequently, 5-axis 3D printers can also be considered for 3D conformal electronics. With the limited number of elemental semiconductors such as Te, Ge and Ga, conjugated polymers and carbon-based materials should be studied to create an impact in the long term using cost-effective and sustainable raw materials. However, with the lower zT performance of organic TE materials, research developments in the areas of chemical functionalization, composites and nano-structuring are required to make organic TE materials feasible for large-scale employment. The complex morphology of organic materials at the nanoscale brings high potential for achieving high zT through nano-structuring. Materials jetting of 1D materials will thus add value to the thermoelectric performance by tailoring the microstructural architecture. Therefore, if fully embraced, materials jetting of thermoelectrics would be a feasible pathway towards efficient self-powered TE devices.

#### DECLARATIONS

Authors' contributions Conceptualization and writing: Zhang D Writing: Sia SA, Solco SFD Supervision and writing: Xu J, Suwardi A

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Not applicable.

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#### **Conflicts of interest**

All authors declared that there are no conflicts of interest.

#### Ethical approval and consent to participate

Not applicable.

#### **Consent for publication**

Not applicable.

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